

DIN 3964/62 / (mm)

**HDM** PROFIL- FLANKENLINIE

F2.583.370W17 Fraesen Mk5Hy Zahnrad LFD. NR.: 30

TYP : F2 BEMERKUNG : 0

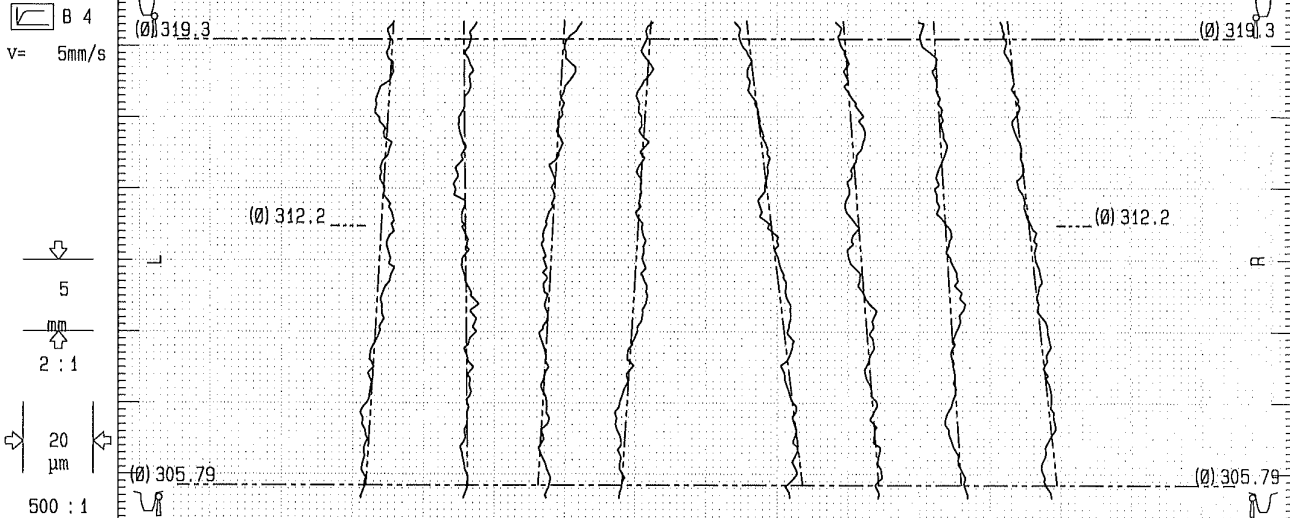
Losnummer 4391793 Arbeitsg. 0400

Bearbmasch

z 75 R/R  $\alpha_n$  12°0'0"  $\phi=1.5/1.5/1.5$ mm  $L_a$  13.51->14.31/13.51->14.31 mm  $d$  310.876/310.876 mm

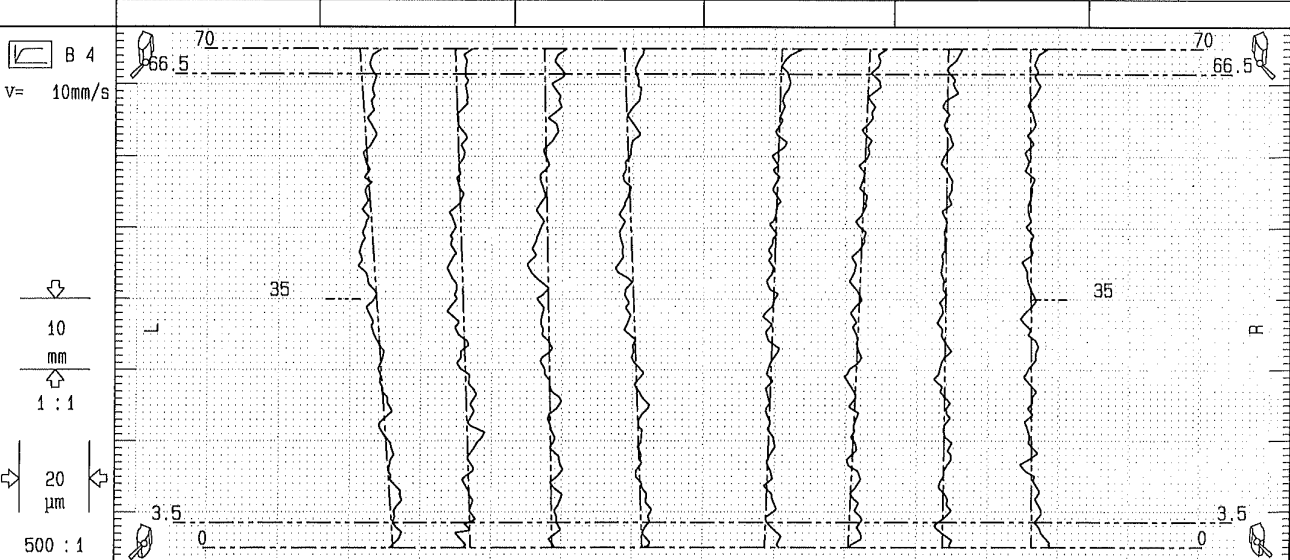
$m_n$  4 mm  $\beta$  15°12'0"/15°12'0"  $b$  70 mm  $d_b$  303.598/303.598 mm \*  $T_p=32.8^\circ C$

NDP 6.35/inch  $\beta_b$  14°51'36"/14°51'36"  $x$  .165  $L_\beta$  90->100/90->100 %  $\frac{1}{2}$   $\frac{1}{4}$   $\frac{1}{8}$



$\Sigma Q$	[...]	$\bar{x}$	Q	58	39	20	1		1	20	39	58	Q	$\bar{x}$	[...]
$\frac{1}{8}$	0/25	9.7	6	9.7	7.2	10.7	11.1	$f_{Fa}$	16	12.1	12.3	14.7	7	13.8	0/25
$\frac{1}{9}$	0/20	7.4	6	8.2	6.9	7	7.3	$f_{Fa}$	7.2	7.6	8	6.5	6	7.3	0/20
	+14	-5.7	7	-7.8	1	-7.5	-8.4	$f_{Ha^*}$	<b>-15.5</b>	-9.9	-7.8	<b>-14.1</b>	9	-11.8	+14
	-/-	-5.7						$f_{HaM}$						-11.8	-/-
	-/-	9.4						$f_{\sigma a}$						7.7	-/-
$\frac{1}{8}$															
$\frac{1}{7}$															

0973



$\Sigma Q$	[...]	$\bar{x}$	Q	58	39	20	1		1	20	39	58	Q	$\bar{x}$	[...]
$\frac{1}{8}$	0/25	11.1	7	12.5	10.7	10.7	10.5	$f_{F\beta}$	10.9	11.7	8	8.6	6	9.8	0/25
$\frac{1}{6}$	0/18	9.8	7	8.8	9.5	11.7	9.3	$f_{F\beta}$	8.5	7.9	7.1	8.5	6	8	0/18
	+20	-5.7	6	-9.9	-4.8	-2.6	-5.4	$f_{H\beta^*}$	4.4	5.8	1.3	-6	5	2.7	+20
	-/-	-5.7						$f_{H\beta M}$						2.7	-/-
	-/-	7.3						$f_{\sigma\beta}$						6.4	-/-
$\frac{1}{8}$															
$\frac{1}{7}$															

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DIN 3961/82 / (mm)

STIRNRAD:

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<b>HDM</b>				<b>TEILUNG</b>																																													
F2.583.370W17 Fraesen Mk5Hy				Zahnrad				LFD. NR.: 30																																									
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z	75	R/R	$\alpha_n$	12° 0' 0"	$\phi = 1.5/1.5/1.5$ mm	$L_a$	13.51->14.31/13.51->14.31 mm	$d$	310.876/310.876 mm																																								
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$v_m =$	10mm/s	$\perp Q$	=Q	[...]																																													
$v_p =$	40mm/s																																																
x																																																	
<div style="display: flex; justify-content: space-between;"> <span>↓ +</span> <span>20 <math>\mu</math>m</span> <span>↑ -</span> </div>																																																	
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td><math>f_p</math></td> <td>8</td> <td>5</td> <td>0/ 20</td> <td>5.1</td> <td>▼ #29</td> <td>▲ #69</td> <td></td> <td></td> <td></td> </tr> <tr> <td><math>f_u</math></td> <td>8</td> <td>4</td> <td>0/ 25</td> <td>5.1</td> <td></td> <td>#29</td> <td></td> <td></td> <td></td> </tr> </table>										$f_p$	8	5	0/ 20	5.1	▼ #29	▲ #69				$f_u$	8	4	0/ 25	5.1		#29																							
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<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td><math>F_p</math></td> <td>8</td> <td>4</td> <td>0/ 80</td> <td>14.9</td> <td>▼ #56</td> <td>▲ #16</td> <td></td> <td></td> <td></td> </tr> <tr> <td><math>F_{pz/8}</math></td> <td>8</td> <td>3</td> <td>0/ 50</td> <td>8.3</td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>										$F_p$	8	4	0/ 80	14.9	▼ #56	▲ #16				$F_{pz/8}$	8	3	0/ 50	8.3																									
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<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td><math>\phi = 6.51 F_r</math></td> <td>8</td> <td>7</td> <td>0/ 56</td> <td>33.3</td> <td>▼ #64</td> <td>▲ #32</td> <td></td> <td></td> <td></td> </tr> </table>										$\phi = 6.51 F_r$	8	7	0/ 56	33.3	▼ #64	▲ #32																																	
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<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td></td> <td><math>\frac{1}{2}</math></td> <td></td> <td></td> <td></td> <td></td> <td><math>\frac{1}{2}</math></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td><math>\frac{1}{2}</math></td> <td>81.33 &lt;= 81.35 &lt;= 81.35</td> <td></td> <td></td> <td></td> <td><math>\frac{1}{2}</math></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td><math>\frac{1}{2}</math></td> <td>81.327 &lt;= 81.333 &lt;= 81.338</td> <td></td> <td></td> <td></td> <td><math>\frac{1}{2}</math></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td>7</td> <td>( aus Teilung )</td> <td></td> <td></td> <td></td> <td><math>\frac{1}{2}</math></td> <td></td> <td></td> <td></td> </tr> </table>											$\frac{1}{2}$					$\frac{1}{2}$					$\frac{1}{2}$	81.33 <= 81.35 <= 81.35				$\frac{1}{2}$					$\frac{1}{2}$	81.327 <= 81.333 <= 81.338				$\frac{1}{2}$					7	( aus Teilung )				$\frac{1}{2}$			
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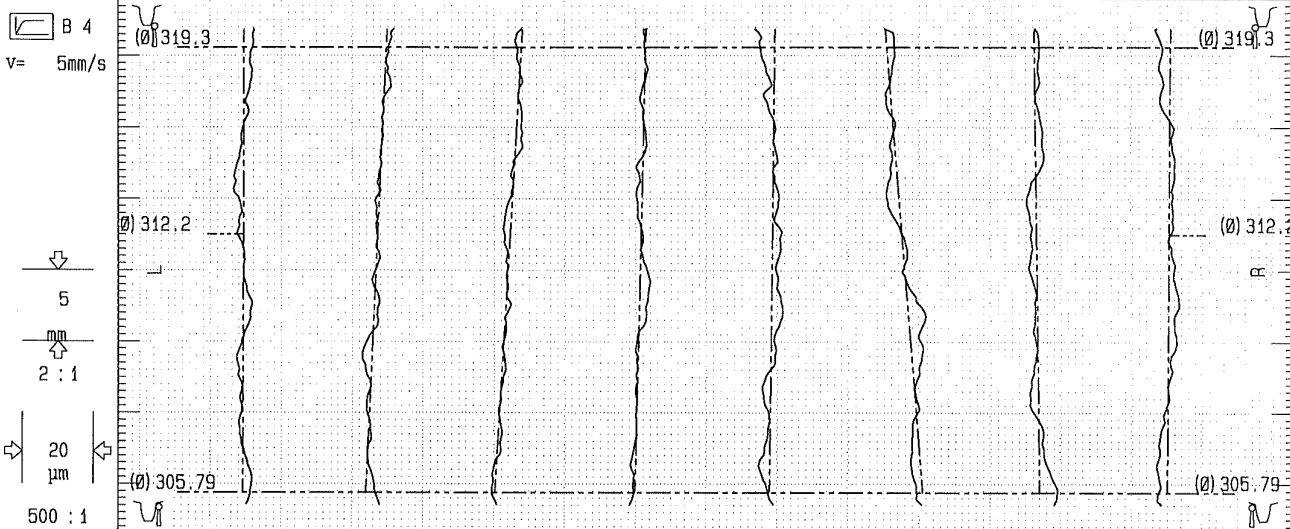
DIN 3961/62 / (mm)



Losnummer 4403683 Arbeitsg. 0400  
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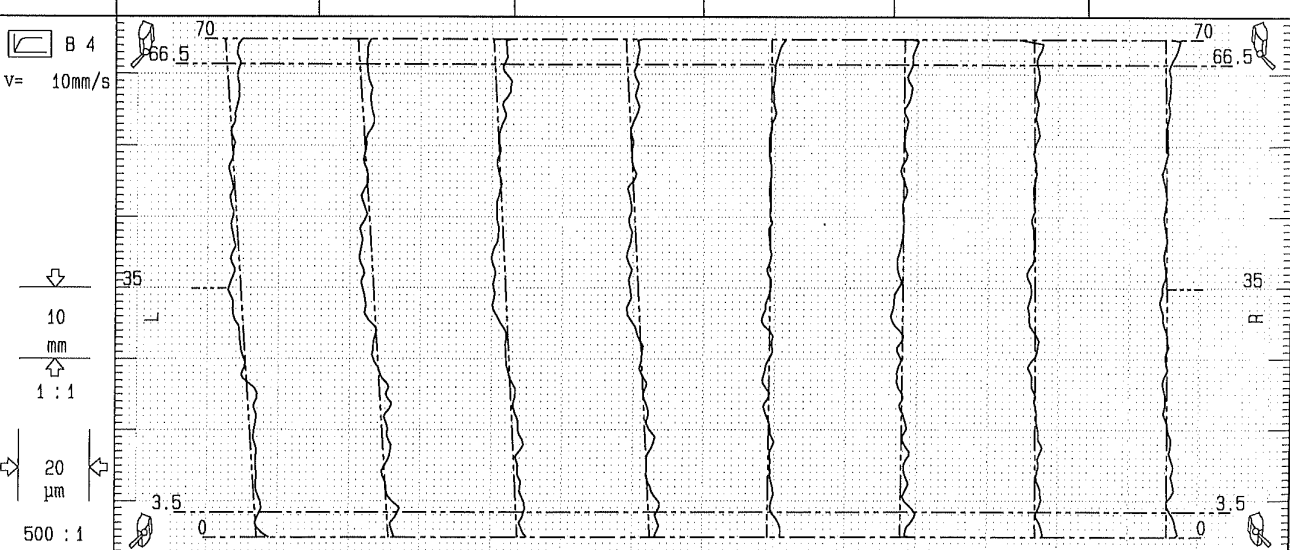
z	75	R/R	$\alpha_n$	12° 0' 0"	$\phi = 1.5/1.5/1.5$ mm	$L_a$	13.51 → 14.31 / 13.51 → 14.31 mm			$d$	310.876 / 310.876 mm
$m_n$	4 mm	$\beta$		15° 12' 0" / 15° 12' 0"	b	70 mm	$d_b$	303.598 / 303.598 mm	*	$T_M = 21.4^\circ C$	
NDP	6.35 / inch	$\beta_b$		14° 51' 36" / 14° 51' 36"	x	.165	$L_\beta$	90 → 100 / 90 → 100 %		$T_A = 21.6^\circ C$	

STIRNRAD:



$\Sigma Q$	[...]	$\bar{x}$	Q	58	39	20	1		1	20	39	58	Q	$\bar{x}$	[...]
	0/25	7.1	5	5.3	8.2	8.9	5.8	$F_a$	6.9	11.3	8.7	6.6	6	8.4	0/25
	0/20	5	5	5.3	5.5	4.2	4.9	$f_{f_a}$	7.2	8.4	7.9	6.4	6	7.5	0/20
	+14	-4.4	7	-3	-6.1	-7.9	-3.3	$f_{H_a^*}$	1.8	-10.3	-1.4	1.2	8	-2.2	+14
	-/-	-4.4						$f_{H_aM}$						-2.2	-/-
	-/-	7.6						$f_{\sigma_a}$						12.1	-/-

B7135 P 40 V7.39 17.01.2014 09:52



$\Sigma Q$	[...]	$\bar{x}$	Q	58	39	20	1		1	20	39	58	Q	$\bar{x}$	[...]
	0/25	10.3	6	9.7	11.7	9.9	9.7	$F_\beta$	4	7.1	4.6	4.2	4	5	0/25
	0/18	7.6	6	7.7	7.2	8.7	6.9	$f_{f_\beta}$	3.8	7.5	4.4	4	6	4.9	0/18
	+20	-8.1	6	-9.2	-9	-7.1	-7.2	$f_{H_\beta^*}$	.9	1	-6	-7	1	.2	+20
	-/-	-8.1						$f_{H_\beta M}$						.2	-/-
	-/-	2.1						$f_{\sigma_\beta}$						1.7	-/-

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